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## Random numbers from vacuum fluctuations

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  - (Received 26 February 2016; accepted 15 July 2016; published online xx xx xxxx)
  - We implement a quantum random number generator based on a balanced homodyne measurement of vacuum fluctuations of the electromagnetic field. The digitized signal is directly processed with
  - a fast randomness extraction scheme based on a linear feedback shift register. The random bit
  - stream is continuously read in a computer at a rate of about 480 Mbit/s and passes an extended test
  - suite for random numbers. *Published by AIP Publishing*. [http://dx.doi.org/10.1063/1.4959887]

Various cryptographic schemes, classical or quantum, require high quality and trusted random numbers for key generation and other aspects of the protocols. In order to keep up with data rates in modern communication schemes, these random numbers need to be generated at a high rate.<sup>1</sup> Equally, large amounts of random numbers are at the core of Monte Carlo simulations.<sup>2</sup> Algorithmically generated pseudo-random numbers are available at very high rates but are deterministic by definition and therefore unsuitable for cryptographic purposes. For applications that require unpredictable random numbers, hardware random number generators have been used in the past<sup>3</sup> and more recently.<sup>4</sup> These involve measuring noisy physical processes and conversion of the outcome into random numbers. Since it is either practically (e.g., for thermal noise sources) or fundamentally impossible to predict the outcome of such measurements, these physically generated random numbers are considered "truly" random.

Quantum random number generators (QRNGs) belong to a class of hardware random number generators where the source of randomness is the fundamentally unpredictable outcome of quantum measurements. Early QRNGs were based on observing the decay statistics of radioactive nuclei. <sup>5,6</sup> More recently, similar QRNGs based on Poisson statistics in optical photon detection have been reported. <sup>7–13</sup> Different schemes use the randomness of a single photon scattered by a beam splitter into either of two output ports. <sup>14,15</sup> As the reflection/transmission of the photon is intrinsically random due to the quantum nature of the process, the unpredictability of the generated numbers is ensured. <sup>16</sup> Other implementations of QRNGs measure the amplified spontaneous emission, <sup>17</sup> the vacuum fluctuations of the electromagnetic field, <sup>18–20</sup> or the intensity <sup>21,22</sup> and phase noise of different light sources. <sup>23–30</sup>

In this paper, we report on a QRNG based on measuring vacuum fluctuations of a light field as the source of ramdomness. <sup>18–20</sup> Such measurements have a very high bandwidth compared to schemes based on photon counting, <sup>7–13</sup> and have a much simpler optical setup compared to phase noise measurements. <sup>23–30</sup> Coupled with an efficient randomness extractor, we obtain an unbiased, uncorrelated stream of random bits at a high rate.

Figure 1 schematically shows the setup of our ORNG. A continuous wave laser (wavelength 780 nm) is used as the local oscillator (LO) for the vacuum fluctuations entering the beam splitter at the empty port. The output of the beam splitter is directed onto two photodiodes, and the photocurrent difference is processed further. This setup is known as a balanced homodyne detector<sup>31,32</sup> and maps the electrical field in the second mode entering the beam splitter to the photocurrent difference  $i_1 - i_2$ . Here, the second input port is empty, so the homodyne measurement is probing the vacuum state of the electromagnetic field. This field fluctuates<sup>33</sup> and is used as the source of randomness. As the vacuum field is independent of external physical quantities, it cannot be tampered with. Since the optical power impinging on the two photodiodes is balanced, any power fluctuation in the local oscillator will be simultaneously detected, and therefore cancel in the photocurrent difference. 32,34 In an alternative view, the laser beam can be seen as generating photocurrents  $i_1$ and  $i_2$  with a shot noise power proportional to the average optical power. The shot noise currents from the diodes add up as they are uncorrelated, while amplitude fluctuations in the laser intensity (referred to as classical noise) do not affect the photocurrent difference.

The power of the two output ports is balanced by rotating the laser diode in front of a polarizing beam splitter 77

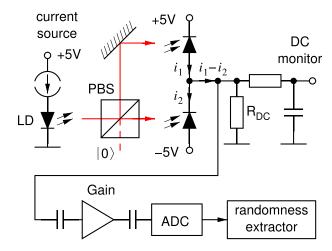


FIG. 1. Schematic of the quantum random number generator. A polarizing beam splitter (PBS) distributes light from a 780 nm laser equally onto two photodiodes, generating photocurrents  $i_1$  and  $i_2$ . The current difference  $i_1 - i_2$  is amplified, digitized, and processed to generate random numbers.

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(PBS). Light leaving the PBS is detected by a pair of reverse biased silicon pin photodiodes (Hamamatsu S5972) connected in series to perform the current subtraction. The balancing of photocurrents is monitored by observing the voltage drop across a resistor  $R_{DC}$  providing a DC path from the common node to ground. We achieve a 50 dB rejection ratio of the classical noise from the laser intensity fluctuations by careful balancing. The fluctuations  $\Delta(i_1 - i_2)$  above 20 MHz are amplified by a transimpedance amplifier (Analog Devices AD8015) followed by two wideband RF gain blocks (Mini Circuits MAR-6). The entire amplifier chain has a calculated effective transimpedance of  $R_{\rm eff} \approx$  $540 \pm 118 \text{ k}\Omega$ .

To ensure that the fluctuations at the amplifier output are dominated by quantum noise, the spectral power density is measured (see Fig. 2). With an optical power of 3.1 mW received by each photodiode corresponding to an average photocurrent I = 1.7 mA, we observe a noise power of P =-53.5 dBm (at 75 MHz) in a bandwidth of B = 1 kHz. This is about 1.5 dB lower than the theoretically expected shot noise value (dashed trace)

$$P = \frac{4eIBR_{\rm eff}^2}{Z} \approx -52 \, \mathrm{dBm},\tag{1}$$

where e is the electron charge and  $Z = 50 \Omega$  the load impedance.<sup>35</sup> The difference is compatible with uncertainties in determining the transimpedance of the amplifier. The measured total noise has a relatively flat power density in the range of 20-120 MHz, with high pass filters in the circuit suppressing low frequency fluctuations. The high end of the pass band is defined by the cutoff frequency of the amplifier. To illustrate the effectiveness of removing classical noise in the photocurrents, the spectral power density of the photocurrent generated from a single diode is also shown. Strong spectral peaks at various radio frequencies appear to enter the system probably via the laser diode current. For completeness, the spectral power density of the electronic noise is recorded without any optical input and found to be at least

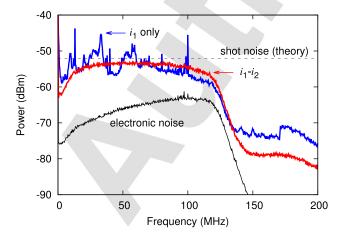


FIG. 2. Amplified noise levels measured into a resolution bandwidth B=1kHz. The total noise is measured from the photocurrent difference  $i_1 - i_2$ with equal optical power impinging on both photodiodes and approaches the theoretical shot noise level of -52 dBm (dashed trace) given by (1). The current  $i_1$  of a single photodiode reveals colored classical noise. The electronic noise is measured without any optical input.

10 dB below the total noise level, i.e., the total noise is dominated by quantum fluctuations.

The amplified total noise is digitized into signed 16 bit 115 words  $x_i$  at a sampling rate of 60 MHz with an analog to digital converter (ADC, Analog Devices AD9269-65). The sam- 117 pling rate is lower than the cut-off frequency of the noise 118 signal to avoid temporal correlation between samples. As 119 shown in Fig. 3, the normalized autocorrelation

$$A(d) = \langle x_i x_{i+d} \rangle_n / \langle x_i^2 \rangle_n, \tag{2}$$

evaluated over  $n = 10^9$  samples shows that the absolute 121 value of the autocorrelation |A(d)| for non-zero delay (d > 0) 122 is below  $1.2\times10^{-3}$ , which is slightly smaller than what has 123 been observed in other experiments. <sup>23,36,37</sup> The residual cor- 124 relation above the  $2\sigma$  confidence level for  $d \leq 60$  is a consequence of the finite bandwidth of the signal, as stated by the 126 Wiener-Khinchin theorem.

The total noise measured before the ADC contains both 128 quantum and electronic noise. To determine how much randomness from the non-classical origin can be safely 130 extracted, it is necessary to estimate the entropy  $H(X_a)$  contributed by the quantum process.

Therefore, we assume that the measured total noise sig- 133 nal  $X_t = X_q + X_e$  is the sum of independent random variables 134  $X_q$  for the quantum noise, and  $X_e$  for the electronic noise 135 which includes the photodetector, amplifier, and digitizer 136 noise. All three variables  $X_q$ ,  $X_e$ , and  $X_t$  are assumed to have discrete values between  $-2^{15}$  and  $2^{15}-1$ . We take the have worst case scenario that an adversary has full knowledge of 139 the electronic noise, i.e., is able to predict the exact outcome 140 of  $X_e$  at any moment. In this case, the amount of quantumbased randomness in the acquired total noise signal is quanti- 142 fied by the conditional entropy  $H(X_t|X_e)$ , i.e., the entropy in 143 the total signal, given full knowledge of the electronic noise 144  $X_e$ . As the variables are assumed to be additive and independent, the conditional entropy is  $H(X_t|X_e) = H(X_q + X_e|X_e)$  146  $=H(X_q|X_e)=H(X_q).$ 

The variance of the total noise,  $\sigma_t^2$ , is given by the sum 148 of the variances  $\sigma_q^2$  for the quantum noise, and  $\sigma_e^2$  for the 149 electronic noise. Over  $10^9$  samples, we find  $\sigma_t = 4504.41$  150 and  $\sigma_e = 1481.8$ , measured with the laser switched off (see 151

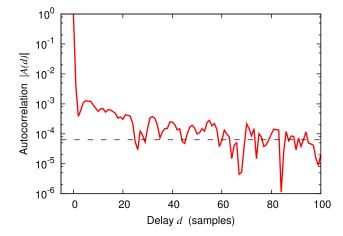


FIG. 3. Autocorrelation of the total noise signal sampled at 60 MHz, computed over  $10^9$  samples (solid line), compared with the  $2\sigma$  confidence level (dashed line).

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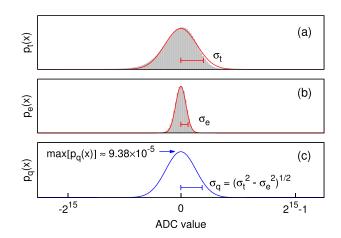


FIG. 4. Probability distribution of the measured total noise with variance  $\sigma_t^2$ (a), electronic noise with variance  $\sigma_e^2$  (b), and the estimated quantum noise with variance  $\sigma_q^2$  (c). The filled areas in (a), (b) show the actual measurements over 10<sup>9</sup> samples, the solid lines fit to Gaussian distributions.

Fig. 4). Note that for the total noise, the observed distribution is slightly skewed compared to a Gaussian distribution [solid 154 line in Fig. 4(a)], possibly due to a distortion in the digitizer. Assuming the quantum noise  $X_q$  has a Gaussian distribution,<sup>33</sup> we would assign a variance  $\sigma_q^2 = \sigma_t^2 - \sigma_e^2 \approx 4253.7^2$ . 156 To estimate the entropy for a Gaussian distribution, we use 157 the Shannon entropy 158

$$H_S(X_q) = \sum_{x=-2^{15}}^{2^{15}-1} -p_q(x) \log_2 p_q(x), \tag{3}$$

where  $p_q(x)$  is the probability distribution of the quantum noise  $X_q$ . Since  $\sigma_q \gg 1$ ,  $H_S(X_q)$  can be well approximated 161

$$\int_{-\infty}^{+\infty} -f(x) \log_2 f(x) dx = \log_2(\sqrt{2\pi e} \,\sigma_q), \tag{4}$$

where f(x) is a Gaussian probability density function with variance  $\sigma_a^2$  and e the base of the natural logarithm.<sup>38</sup> This 163 yields 14.1 bits of entropy per 16 bit sample. We also evalu-165 ate the min-entropy of this distribution

$$H_{\infty}(X_q) = -\log_2(\max[p_q(x)]) \approx \log_2(\sqrt{2\pi}\sigma_q), \quad (5)$$

where  $\max[p_q(x)]$  is the maximum value of the probability distribution of  $X_a$ . This yields a min-entropy of 13.4 bits per 167 168

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The Shannon entropy  $H_S(X_q)$  serves as an upper bound of extractable randomness, while the min-entropy sets a lower bound, i.e., the least amount of randomness possessed by each sample. An alternative estimation of the entropy in  $X_a$  assumes that electronic noise is not only known to a third party but also could be tampered with. 19,36,39

In many applications, random numbers are required to be not only unpredictable but also uniformly distributed. As such, the raw ADC output cannot be directly used. Randomness extractors convert non-uniformly distributed raw data into a uniformly distributed binary stream without correlations. 40 Although there is no deterministic universal

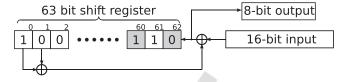


FIG. 5. Schematic of a LFSR-based randomness extractor. Eight bits (from the shaded positions) are extracted for every 16 bits of input.

randomness extractor, 40 various practical implementations 181 have been reported. Examples are Trevisan's extractor, a 182 Toeplitz hashing extractor,<sup>37</sup> random matrix multiplica- 183 tions,<sup>22,41</sup> or a family of secure hashing algorithms (SHA).<sup>18</sup> 184

In this work, we use a randomness extractor based on a 185 Linear Feedback Shift Register (LFSR) as shown in Figs. 5 186 and 6, equivalent to a cyclic redundancy check (CRC). 42 The 187 LFSRs are well known for generating long pseudo-random 188 streams with little computational resources and are in widespread use in communication applications for spectrum 190 whitening. 43-47

We use a maximum length LFSR with 63 cells and a 192 two-element feedback path. Its state at any time t is a row 193 vector  $S_t$  of 63 bits, with a recursion relation

$$S_{t+1} = S_t M + R_t$$

$$= (s_0, s_1, s_2, \dots s_{62}) \begin{pmatrix} 0 & 0 & \cdots & 0 & 1 \\ 1 & 0 & \cdots & 0 & 1 \\ 0 & 1 & \cdots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \cdots & 1 & 0 \end{pmatrix}$$

$$+ (0, 0, 0, \cdots 0, r_t)$$
  
=  $(s_1, s_2, s_3, \cdots s_{62}, s_0 + s_1 + r_t),$  (6)

where an elementary addition represents a binary xor, and a 195 multiplication a binary and operation.

The  $63 \times 63$  matrix M represents the shift and feedback 197 operation on the LFSR state. The addition of row vector  $R_t$  198 describes the injection of one raw random bit  $r_t$  into  $S_t$ . After 199 *n* cycles, the LFSR state becomes

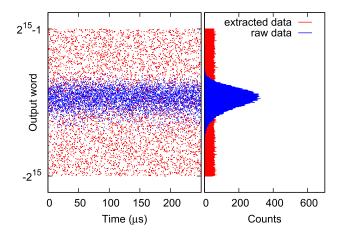


FIG. 6. Distribution of random data before (blue) and after (red) the randomness extractor, shown in time domain (left) and histogram (right).

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$$S_{t+n} = S_t M^n + \underbrace{R_t M^{n-1} + \dots + R_{t+n-1}}_{A} . \tag{7}$$

201 Row vector A can be expressed as a matrix product

$$A = (r_t, r_{t+1}, \cdots, r_{t+n-1})T,$$
 (8)

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$$T = \begin{pmatrix} S'M^{n-1} \\ S'M^{n-2} \\ \vdots \\ S'I \end{pmatrix}, \quad S' = (0, 0, \dots 0, 1). \quad (9)$$

Matrix T in (9) is a  $63 \times 63$  Toeplitz matrix with rows generated from a LFSR sequence (6) with  $R_t = 0$  and initial state  $S_t = S'$ . It was shown that multiplying an input stream by such a Toeplitz matrix can be used as a hashing function that generates an almost-uniform output.<sup>43</sup>

In our setup, we serially inject the 16 bits from each ADC output word into the LFSR but extract only 8 bits  $s_i$  provided by stream  $S_t$  (at positions 62, 60, ..., 48 after the injection) in a parallelized topology. This is equivalent to a privacy amplification process<sup>48</sup> and ensures that no residual correlations due to the non-uniform input distribution or any classical noise that may be known to an adversary are present in the output stream, because the extraction ratio of 50% is lower than the  $13.4/16 \approx 84\%$  allowed by the min entropy (5).

A merit of this extractor is its low complexity. Unlike many other secure hashing algorithms, it can be easily implemented either in high speed or low power technology. Therefore, the extraction process does not limit the random number generation rate. This scheme can be parallelized using 126 register cells, capable of receiving up to 63 injected raw bits per clock cycle while still following the extractor equation (6). With a CPLD operating at a clock frequency of 400 MHz, this algorithm would be able to process up to  $25 \times 10^9$  raw input bits per second.

To evaluate the quality of the extracted random numbers, we apply two suites of randomness tests: the statistical test suite from NIST<sup>49</sup> and the "Die-harder" randomness test battery.<sup>50</sup> The output of our RNG passed both tests consistently when evaluated over a sample of 400 Gigabit in the sense that occasional weak outcomes of some tests do not repeat.

Our implementation has an output rate of about 480 Mbit/s of uniformly distributed random bits, with the digitizer unit sampling at 60 MHz and randomness extraction ratio of 50%; this is limited by the speed of the data transmission protocol (USB2.0). While significantly higher generation rates have been reported recently, <sup>17,23,25</sup> our design in comparison is simpler both in hard- and software implementation. With moderate effort, our random number generation rate can be greatly increased by extending the bandwidth of the photodiodes, amplifiers, and digitizer devices, while maintaining the relatively simple randomness extraction mechanism. Practically, the resolution-bandwidth product of the ADC limits the random bit generation rate.

In summary, we demonstrated a random number generation scheme by measuring the vacuum fluctuations of the electromagnetic field. By estimating the amount of usable entropy

from quantum noise and using an efficient randomness extrac- 249 tor based on a linear feedback shift register, we can generate 250 uniformly distributed random numbers at a high rate from a 251 fundamentally unpredictable quantum measurement.

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<sup>38</sup>One can show that  $|H(X_q) - H'(X_q)| < \log_2(\sqrt{2\pi}\sigma_q)/(\sqrt{2\pi}\sigma_q) \approx 0.0013$  319 bit for  $\sigma_q = 4108$ .

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